

# Liquid Fuel Fire Hazard Characterization

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# Background

## ■ Liquid Fuel Fires

- Potential hazard in many applications
- Nature of the accident is highly variable
  - Source of release
  - Surface features (e.g., concrete, ground, water)
  - Confinement of spill
  - Point of ignition



# General Characterization

- Continuously Flowing Spill
- Instantaneous Spill / Pool (static)
  - Unconfined spill fire
  - Confined pool fire (typically greater fuel depth)



# Hazard Analysis Objectives

- Determine impact of a fire on surroundings:
  - 1 Does the fire directly impinge on objects (e.g., roof members, equipment, aircraft)?
  - 2 What is the radiant heat transfer to targets?



# Specific Goals

- Determine physical size of fire
  - Spill area (base of fire)
  - Flame height
- Determine heat release rate,  $\dot{Q}$
- Based on physical fire size or  $\dot{Q}$ , estimate radiant flux to targets



# Typical Calculations

Heat Release Rate (kW):  $\dot{Q} = \dot{m} \cdot \Delta h_c$

Burning Rate (kg/m<sup>2</sup>s):  $\dot{m} = A \cdot \dot{m}''$

Mass burning rate per area is empirically based.

Burning Rate (kg/m<sup>2</sup>s):  $\dot{m} = A \cdot \dot{y} \cdot \rho$

Density,  $\rho$ , is known and

Regression rate is empirically based.



# Area of Static Fuel Release

- A is known via physical constraints  
or
- A is calculated based on the initial volume of fuel,  $V$ , and an estimated spill depth,  $\delta$ :

$$A = \frac{V}{\delta}$$



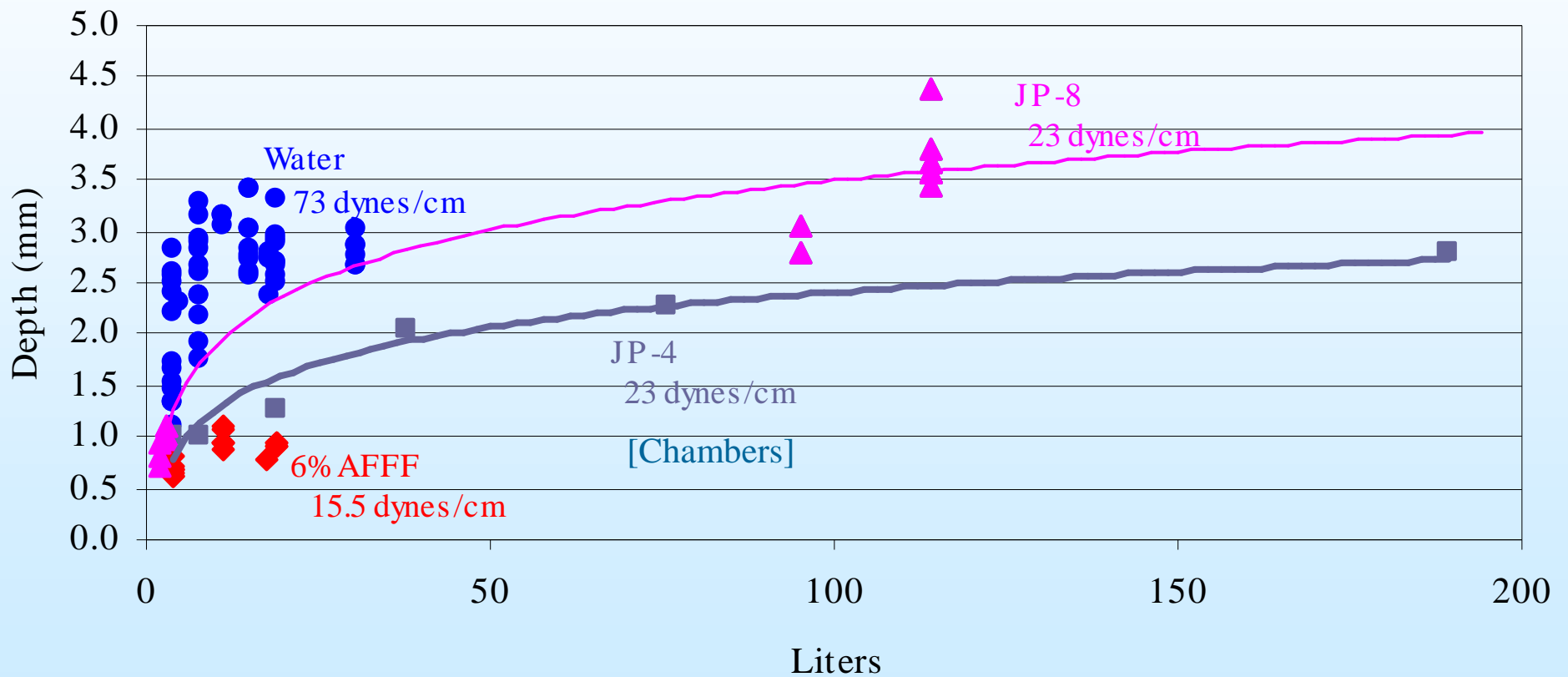
# Estimate of Spill Depth

- MacKinven et al (1970) and Burgoyne and Roberts (1968) work indicate
  - No flame spread for Depths < 1.5 mm
- Experimental data for JP-8 and JP-4 fuels indicate depths as low as 0.7 mm
- Smaller depth -- larger spill area -- larger fire -- shorter duration (all other things constant)

$$\dot{Q} = \dot{m}'' \cdot A \cdot \Delta h_c = \dot{m}'' \cdot V / \delta \cdot \Delta h_c$$



# Liquid Spill Depths on Concrete



# Estimated Minimum Spill Depths

Spill < 95 L (25 gal)	Depth = 0.7 mm
Spill ≥ 95 L (25 gal)	Depth = 2.8 mm

Alternately, express as the spill area per volume of fuel:

Spill < 95 L (25 gal)	$A/V = 1.4 \text{ m}^2/\text{L}$ (57 ft <sup>2</sup> /gal)
Spill ≥ 95 L (25 gal)	$A/V = 0.36 \text{ m}^2/\text{L}$ (15 ft <sup>2</sup> /gal)



# Area of Continuously Flowing Unconfined Spill Fire

Maximum spill area based on balance between volumetric flow rate and volumetric burning rate of fuel:

$$\dot{V}_L = A \cdot \dot{y} = \frac{\Pi D^2}{4} \dot{y}$$



# Continuously Flowing Unconfined Spill Fire

- Area also can be estimated using experimental correlations
- Mansfield and Linley [1991]:

$$D = 3.5\dot{V}^{1/2}$$

D = spill diameter (ft)

V = spill rate (gpm)

Correlation is best fit to 150 to 600 gpm spill data

Uncertainty estimated at  $\pm 20\%$



# Typical Calculations

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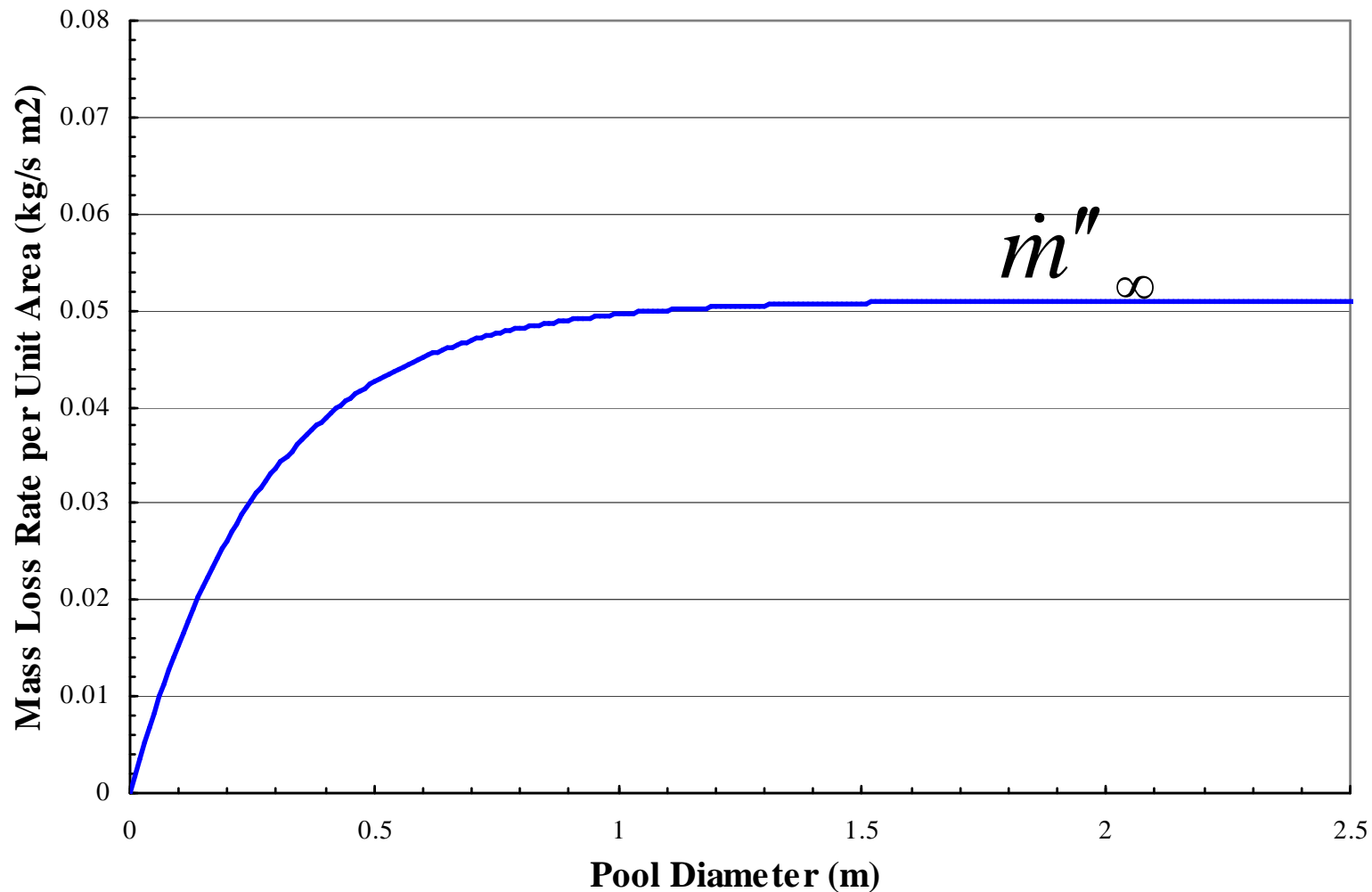
# Flame Spread Rate

- Temperature of liquid most important factor
- Gas-phase ( $20\text{ C} > T_{\text{FP}}$ )
  - 130 to 220 cm/s
- Liquid-phase
  - 1 to 12 cm/s
- Spread on porous surfaces
  - cm/min



# Pool Correlation

$$\dot{m}'' = \dot{m}''_{\infty} \left( 1 - e^{-k\beta D} \right)$$



# Issues

- Most published data is for confined fires (pan or diked pools)
- Pool depths typically greater than spill depths
- Will the pool fire correlation (or available regression rate data) accurately predict spill fire burning rates?
- How well can we estimate spill fire heat release rates and flame heights?

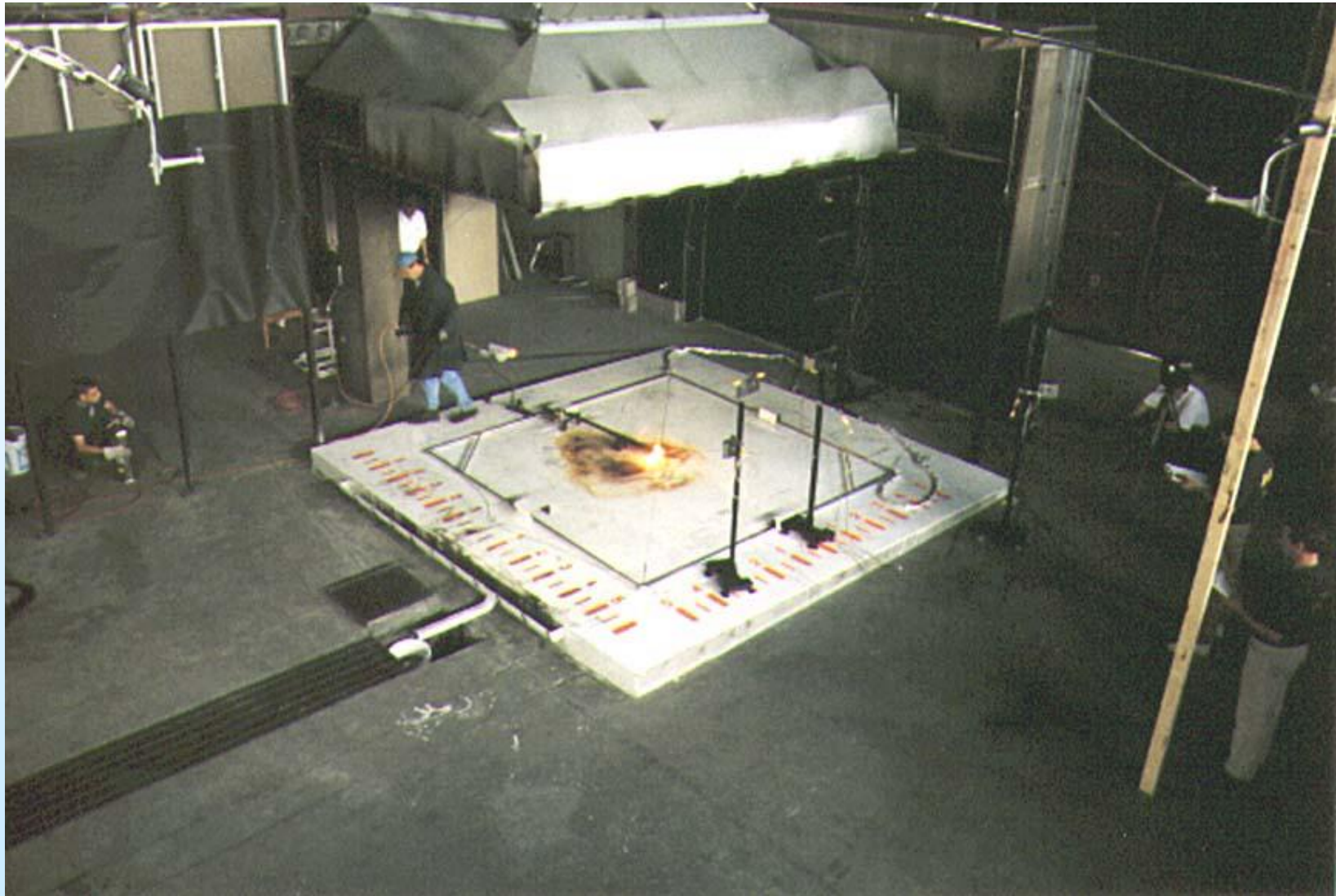


# Experimental Program

- Measured pool size and HRR of JP-8 and JP-5 spill fires → calculated burning rate
- Scenarios
  - Unconfined continuous spill, ignition at source
  - Confined (channeled) continuous spill, ignition at source
  - Unconfined fixed quantity, ignition at edge of spill after static



# Experimental Setup



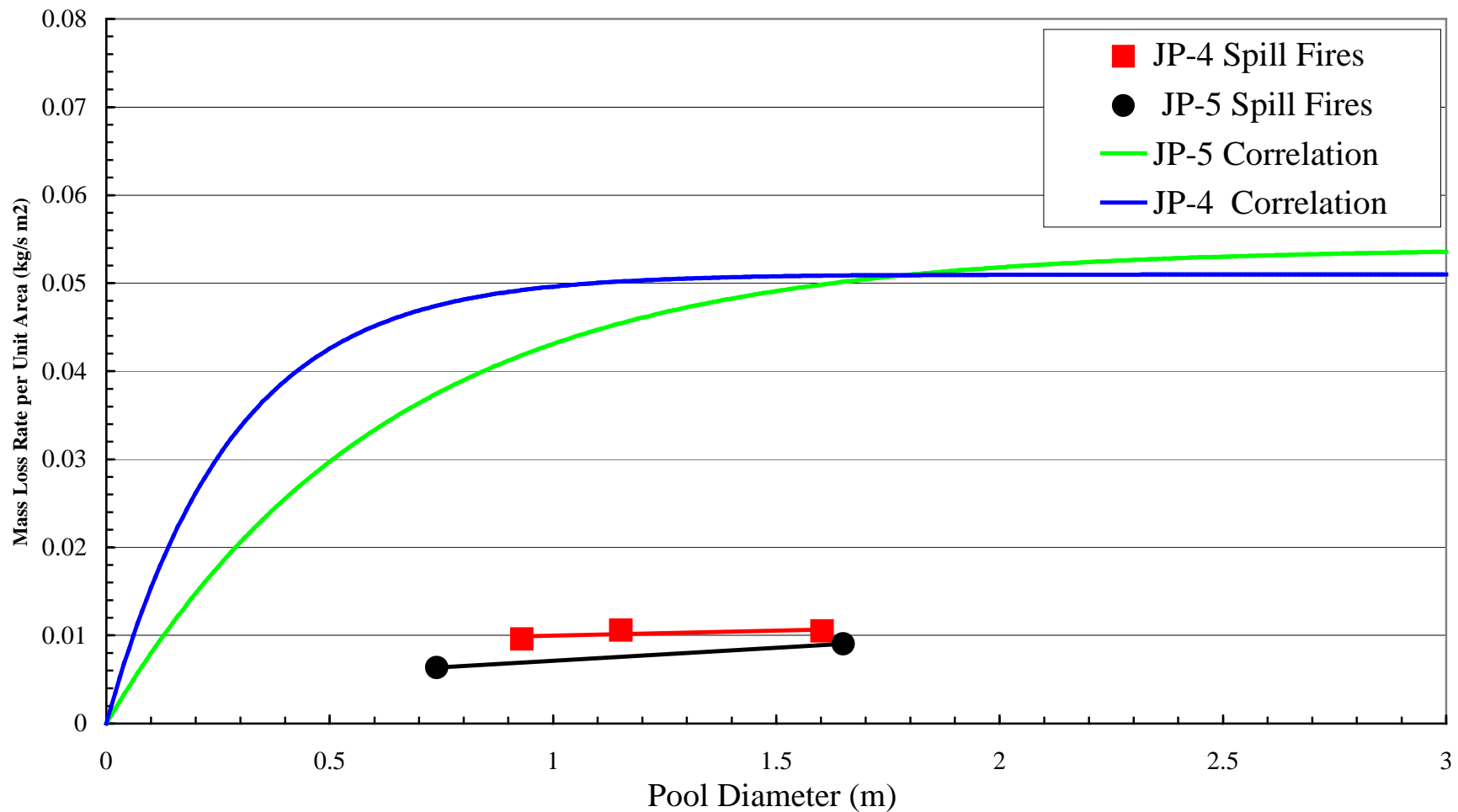
# Typical Unconfined Spill Fire



# Fixed Quantity Spill Fire



# Experimental Fuel Spill Fire Results compared to Pool Fire Correlation



# Findings

- Spill  $\dot{m}''$  approximately 20-25% of the frequently used pool fire data:
  - Navy data
  - Putorti [2000]
- Lower spill fire burning rate correlates to spill diameters ~ twice as large as would be estimated using pool fire data



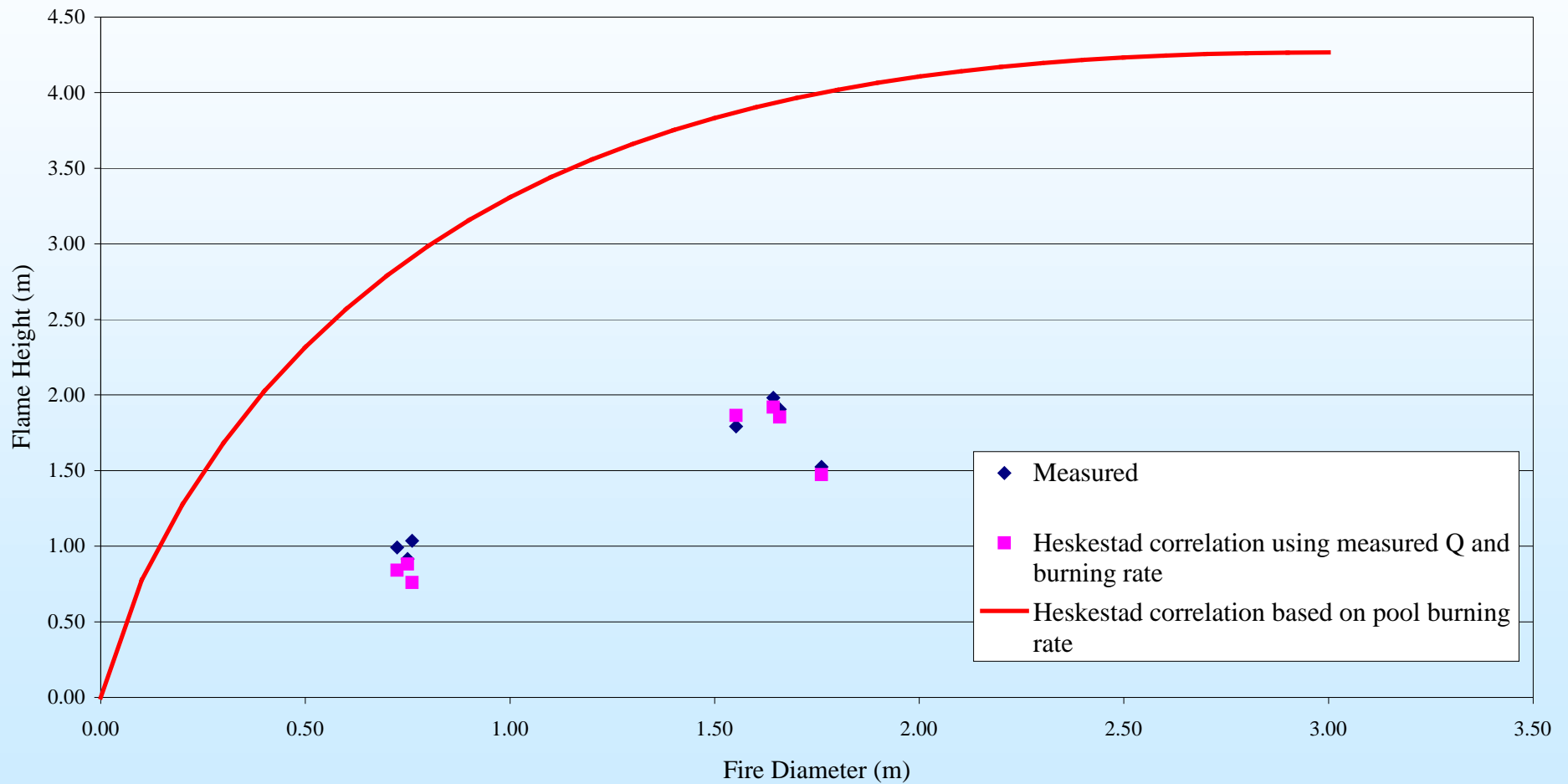
# Flame Height

- Heskestad correlation for intermittent flame height,  $L_f$ :

$$L_f = 0.23\dot{Q}^{2/5} - 1.02D$$



# Flame Height for JP-5 Spill Fires



# Radiant Heating of Targets

- Shokri and Beyler Method

$$q'' = E \cdot F_{1-2}$$

$$E = 58(10^{-0.00823 \cdot D}) = [kW / m^2]$$



# Conclusions

- Experiments demonstrated that commonly used pool fire data is not accurate for predicting fuel spill fire dynamics
- Average depths for spills can be as small as 0.7 to 1.1 mm



# Conclusions

- Spill  $\dot{m}''$  approximately 20-25% of the frequently used pool fire data
- Use of lower spill fire burning rates results in spill diameters ~ twice as large as would be estimated using pool fire data



# Conclusions

- The Heskestad intermittent flame height correlation accurately predicts  $L_f$  when using the correct spill or pool fire burning rate

